

JUNE 15, 1918

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# AVIATION AND AERONAUTICAL ENGINEERING



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VOLUME IV  
Number 10

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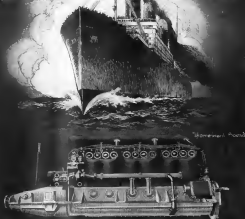
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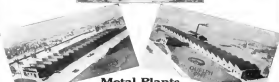
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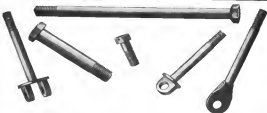
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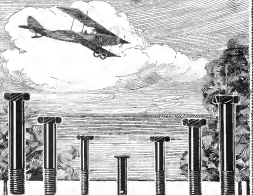
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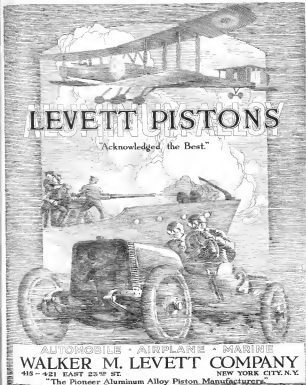
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Total Assets.....	\$13,422,862.51
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Capital.....	2,000,000.00
Net Surplus to Policyholders....	6,232,068.87

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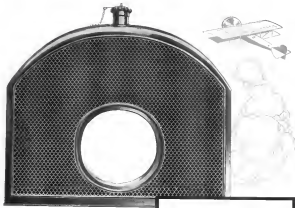
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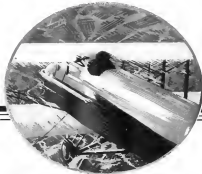
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JUNE 15, 1918

# AVIATION AND AERONAUTICAL ENGINEERING

VOL. IV. NO. 10

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## INDEX TO CONTENTS

PAGE	PAGE
The Importance of Numbers in Aerial Warfare .....	694
The 240 H.P. 8 Cylinder Mercedes Engine .....	698
Machine Guns for American Aircraft .....	699
Digest of the Foreign Aeronautical Press .....	682
The Model M T 2 Larsson Biplane .....	692
News of the Forthright .....	685

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ISSUED ON THE FIRST AND FIFTEENTH OF EACH MONTH FORMERLY CLOSELY PREVIOUSLY ENTERED AS SECOND CLASS MATTER AUGUST 5, 1915, AT THE POST OFFICE OF NEW YORK, N. Y., UNDER ACT OF MARCH 3, 1879.

## EFFICIENT AERIAL NAVIGATION DEPENDS UPON

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bers of group 1 is proportional to the surviving numbers of group 2, and that the rate of decrease in the numbers of group 2 is proportional to the surviving numbers in group 1. The ability or quality of the two groups is indicated in the proportionality factors  $A$  and  $B$ .

Differentiating, once and substituting from the original equations, we obtain

$$\frac{dx}{dt} = Ax - Bx \quad \frac{dy}{dt} = Ay - Bx \quad (2)$$

If we let  $Ax = X$ , the relation of these familiar equations may be written:

$$\frac{dX}{dt} = X - Bx \quad \frac{dY}{dt} = Y - Bx \quad (3)$$

It remains to evaluate the four constants of integration.

When  $t = 0$ ,  $x = A$ ,  $y = 0$   
as that  $x = 0$ ,  $y = B$   
Since  $C_1 = 0$ ,  $C_2 = 0$

as that  $C_1 = 0$ ,  $C_2 = 0$

as that  $C_1 = 0$ ,  $C_2 = 0$

Similarly  $C_1 = 0$ ,  $C_2 = 0$

The general equations expressing the course of events then become

$$x = A \cosh At - B \int_0^t \cosh At \, dt \quad (4)$$

$$y = B \cosh At - A \int_0^t \cosh At \, dt$$

The solutions are symmetrical functions of  $t = \sqrt{AB} \ln 2$ , hence in order to obtain results comparable as the time elapses, we shall maintain constant the product  $AB$  as we vary  $A$  and  $B$  separately.

We shall assume throughout that  $A > B$ .  
There are three cases of interest, namely:

$A < B$ ,  $A = B$ ,  $A > B$

For numerical comparisons let  $A = 2000$ ,  $B = 1000$ .  
We shall keep  $A \cdot B$  constant and equal to 1, in which case the general equations are:

$$x = A \cosh t - B \sinh t \quad (5)$$

$$y = B \cosh t - A \sinh t$$

Let  $A = \frac{1}{2}B$ , hence here  $AB = 1$ ,  $A = 707$ ,  $B = 1.414$ .  
The numerical equations are:

$$x = 2000 \cosh t - 1.414 \sinh t$$

$$y = 1000 \cosh t - 1.414 \sinh t$$

When  $y = 0$ , that is when the enemy squadron is completely destroyed,  $\sinh t = 707$  and  $t = .561$  units. For 561 units of  $t$ ,  $x = 1415$ . Hence while group 1 lost 1000 machines, group 2 lost 561 although group 1 had only half the ability or quality of group 2.

Let  $A = \frac{1}{2}B$ , so that  $A = .315$ ,  $B = 1.204$ .  
The equations are:

$$x = 2000 \cosh t - 1.204 \sinh t$$

$$y = 1000 \cosh t - 1.204 \sinh t$$

When  $y = 0$ ,  $\sinh t = 632.5$  and  $t = .717$  units.  
For this value of  $t$ ,  $x = 1560$ .

Therefore, group 1 has totally destroyed group 2 with a loss of 415 machines only, just because of numerical superiority.

Let  $A = B$ , equal quality,  $A = 1$ ,  $B = 1$ .  
For this case:

$$x = 2000 \cosh t - 1000 \sinh t$$

$$y = 1000 \cosh t - 1000 \sinh t$$

When  $y = 0$ ,  $\sinh t = .500$  and  $t = .50$  units.  
When  $t = .50$

$x = 1732$

So that when the second group was totally destroyed, the remaining 1732 machines in the first group, the one still having a loss of only 268 to the enemy's 1000.

Case IV  
 $A = \frac{1}{2}B$ , greater numbers, better quality  $A = 1.254$ ,  $B = .815$

$x = 2000 \cosh t - .815 \sinh t$   
 $y = 1000 \cosh t - .815 \sinh t$

When  $y = 0$ ,  $\sinh t = .603$  and  $t = .530$  units.  
When  $t$  has this value  $x = 1828$

The first group suffered a loss of only 174 to 1000 of the second.

Case V  
 $A = 2B$ ,  $A = 1.414$ ,  $B = 707$   
 $x = 2000 \cosh t - 707 \sinh t$   
 $y = 1000 \cosh t - 707 \sinh t$

When  $y = 0$ ,  $\sinh t = 0.303$  and  $t = 0.303$  units.  
 $x = 1874$

a loss of only 120 machines.

The following table summarizes the foregoing results:

	Group 1	Group 2
	Initial Number 2000	Initial Number 1000
Case I	1415	561
Case II	1560	415
Case III	1732	268
Case IV	1828	174
Case V	1874	120

The curves, delineated in the accompanying figure, show the numbers fallen out in the two groups after fighting begins. The curves intersect at  $t = \sqrt{AB} \ln 2$ , or in this case at  $t = .561$  units, or at the corresponding value of group 2 machines are 561.

This table shows conclusively that numerical superiority is the controlling factor in every war considered even with the quality factor assumed 1. This fact is especially interesting in this respect where a number of machines fighting on half that number lost of time the quality was out with a loss of 561, as compared to a loss of 1000, in the smaller group.

With these equations it is, of course, possible to calculate the advantage to be derived by separating by superior numbers, the equally numerous enemy group into two groups, and separately annihilating them.

For example a force  $x$  of 1000 units represents a force  $y$  of 500. The result is that the 500 are destroyed with a loss of only 561 to the  $x$  force. This leaves 439  $x$  forces equal to 500 new  $y$  forces which they can destroy with a loss to themselves only 150 units, making a total loss to the  $x$  force of only 268 against 1000 enemy forces.

Consider two unequal groups  $x$  and  $y$  and let us define for relation that must exist between the quality factors  $A$  and  $B$  so that both groups lose simultaneously, all of their machines, or 100% loss.

The general equations are for this assumption

$$x = A \cosh T - B \sinh T$$

$$y = B \cosh T - A \sinh T$$

where  $T$  is the time at which both groups and the ratio of  $T$  is to be determined. By dividing one equation by the other, we get immediately

$$\frac{x}{y} = \frac{A}{B} = \left(\frac{A}{B}\right)^T$$

In other words, in order to overcome a numerical superiority  $\frac{x}{y}$ , the smaller group must have a quality better than the larger group as the square of that ratio. Specifically, to overcome a two to one ratio, the quality of the smaller must be four times that of the larger. A superiority in numbers of three would require a quality of war and so on.

Laplace's demonstration of this principle, which he calls the law of war, and is given below. Our demonstration makes it a special case of the general integrated equations.

The assumption in that two forces are engaged, that

relative strength is measured by the same fraction of both as simultaneously put out of action, that is

$$\frac{dx}{dt} = -\frac{dy}{dt}$$

which, together with

$$x = A \cosh T - B \sinh T$$

gives immediately  $R^2 = A^2$

so, we can say, "the fighting strength of two opposing forces are equal when the products of the qualities by the square of the number respectively are equal."

The time  $T$  at which total destruction is completed is given by

$$\sinh T = \frac{A}{B}$$

Hence, of course, it is necessary to know the absolute quality in order to compute specifically the time, but if the ratio  $A/B$  is as stated above, both groups will eventually completely destroy each other.

It is of more interest to determine what the quality ratio should be in order that when the weaker group is annihilated, the stronger shall have lost the same number of machines.

The condition for this case is, that when

$$x = 0 \quad y = A \cosh T - B \sinh T$$

$$0 = B \cosh T - A \sinh T$$

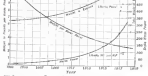
The equations become

$$x = 0 \quad y = A \cosh T - B \sinh T$$

$$0 = B \cosh T - A \sinh T$$

The average horsepower of the Liberty engine has been increased by the National Advisory Commission for Aeronautics.

The first non-military airplane flight was made in December, 1903, with the Wright Brothers' engine developed under 12 hp and weighing 150 lb, or 12.7 hp per horsepower. In 1917, seven years later, the average horsepower of automobile engines had increased to 34 and the weight decreased to 5.7 lb.



per horsepower. In another seven years, 1917, the average power output had advanced to 341 hp, and the weight decreased to 3.2 lb, per horsepower. In March, 1918, the Liberty engine developed 432 hp for a weight of 808 lb, or 156 hp per horsepower. At the present time, May, 1918, the Liberty engine is weighing a maximum of 456 lb for a weight of 825 hp, or 1.84 lb per horsepower.

The accompanying table and curves show the advance in the engine-power-weight ratio by years for the engines in actual service. It is to be especially noted that the Liberty engine, built in 1903, was one year ahead of its time in the matter of power output and weight placed in its weight per horsepower.

In 1917, the Liberty "twelve" was only five per cent more

From the last we get

$$\sinh T = \frac{A}{B}$$

From the second

$$\frac{A}{B} = \cosh T - \sinh T \cosh T$$

so that  $\cosh T = \frac{A}{B}$

Since  $1 - \sinh^2 T = \frac{1}{\cosh^2 T}$  we get, taking  $\frac{A}{B} = x$  the odds,

$$1 - (x^2 - 1) = \frac{1}{x^2}$$

So that, if the odds are 2 to 1 against the smaller group, it will, nevertheless, defeat an equal loss on the larger group if its quality is three times that of the enemy. If the odds are 3 to 1, it must have a superiority of quality 5 in order to destroy an equal number of machines.

Thus, in the military service, where inferior machines are utilized for an equal number of better quality.

Although the treatment of the subject is slightly different from that of Laplace, no change of nomenclature is made by the writers of this article who feel justified in it with at least attention to the fact as clearly brought out that "numbers" certainly do "count."

## Evolution of the Airplane Engine

powerful and twenty-eight per cent lighter per horsepower than the engine of 1903. The average horsepower of the Liberty engine has been increased by the National Advisory Commission for Aeronautics.

The first non-military airplane flight was made in December, 1903, with the Wright Brothers' engine developed under 12 hp and weighing 150 lb, or 12.7 hp per horsepower. In 1917, seven years later, the average horsepower of automobile engines had increased to 34 and the weight decreased to 5.7 lb.

Year of Design	Year	Power	Weight	Weight per Horsepower
1903	1903	12	150	12.5
1904	1904	15	180	12.0
1905	1905	20	240	12.0
1906	1906	25	300	12.0
1907	1907	30	360	12.0
1908	1908	35	420	12.0
1909	1909	40	480	12.0
1910	1910	45	540	12.0
1911	1911	50	600	12.0
1912	1912	55	660	12.0
1913	1913	60	720	12.0
1914	1914	65	780	12.0
1915	1915	70	840	12.0
1916	1916	75	900	12.0
1917	1917	80	960	12.0
1918	1918	85	1020	12.0

The average consumption of oil decreased from about 8 lb per horsepower in 1903 to about 4.5 lb in 1917, or a decrease of about 44 per cent. The average consumption of oil has been steadily dropping to 4.5 lb in 1917, or a decrease of about 44 per cent. The present Liberty consumption is approximately 4.5 lb per horsepower.

Manufacturing the advance made, the Liberty Company in 1917, could only obtain 147 hp at 1600 revolutions per minute from eight cylinders, five from five in diameter, or 18.75 hp per cylinder. This is the same as the Liberty engine which now gives 456 hp, at 1600 revolutions, from twelve cylinders, or 38.0 hp per cylinder obtained in the Liberty engine. Since the Liberty engine is the same as the Liberty engine which, in 1906 revolution, the Liberty engine represents a great advance, for it that speed 250 horsepower are developed, or 28.2 hp per cylinder. Moreover, for the Liberty at the same speed, or 1400 rpm.

Robert's Note: While the above statement is quite interesting, it is not entirely correct. The engine data which is "average on the market" from 1913 to 1917 has been obtained are not necessarily pertinent, for this would greatly reduce the value of the table. One might also point out that the Liberty engine of 1903 was a four-cylinder engine for purposes of comparison with the Liberty engine, cannot be called a representative of its period, for it was never commercially used in any type of airplane. One is also under the impression that the general down model of the Liberty engine, developing 400 hp, was only an experimental type and will not be manufactured for use in service airplanes.]







# The Model M.T.2 Lawson Biplane

Construction was given to the machine easily to obtain strength, but strong, light, and trim. It can also be used for primary glider work, since the rear seat is so arranged as to allow mounting of gliders on the rear of the fuselage. Care was also taken in strengthening all joints, so that the machine has been accomplished to such an extent that the

monogony never leaves the nose of the upper surface of both wings while the rear is placed between the standard ribs from the upper trailing edge to the front spar.

Between the ribs are braced by struts which the legs are supported by separate section spars which do not



THREE-QUARTER FRONT VIEW

usual trouble found in moving parts required for inspection is entirely dispensed with.

The characteristics of the M.T.2 are approximately the following:

Span, upper plane	78 ft.
Span, lower plane	78 ft.
Wing area, upper plane	1,200 sq. ft.
Wing area, lower plane	1,200 sq. ft.
Wing area, total	2,400 sq. ft.
Wing span, total	156 ft.
Wing span, lower plane	78 ft.
Wing span, upper plane	78 ft.
Wing span, total	156 ft.
Wing span, lower plane	78 ft.
Wing span, upper plane	78 ft.
Wing span, total	156 ft.
Wing span, lower plane	78 ft.
Wing span, upper plane	78 ft.
Wing span, total	156 ft.

PLAN

Both wings are in two sections, the top attaching by hinges to wing pins secured in the fuselage and the lower to pins secured in struts and arms to tubes in the body.

The spars are of I-section shape and are bolted at both extremities and extend from attaching points and also wherever any hole occurs such as for the wing and aileron hinges. The ribs are built of laminated wood, reinforced with steel strips between lightening holes, and spaced at regular intervals.



THREE-QUARTER REAR VIEW

body where they connect to a chain and are secured to each other as well.

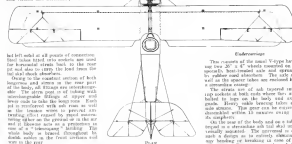
The cables are entirely of steel. The legs are of aluminum section welded directly to the connecting tube and further braced by corner plates. On the lower side of the legs are



corner plates which are so made to prevent any sliding and to also locate each upon assembly. To carry the wings, hook pins are welded in through each end of the connecting tube, which are provided to enter the main landing wire tension. Both front and rear ends of this tube are equipped with air-release rose and tail piece. The front legs of the cables also carry the radiator head plate.

## Body

The fuselage and vertical struts are of ash in front and spruce in the rear. The fuselage is built up of three complete lengths while all struts, both vertical and horizontal, have been channelled.



but left side at all points of connection. Steel tubes fitted to the main and used for horizontal struts back to the rear pit and also to carry the load from the tail shock absorbers.

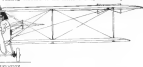
Due to the constant action of both fuselage and struts in the rear part of the body, all struts are interchangeable. The struts are of tubing with interchangeable fittings at upper and lower ends to take the wing ends. Each pit is reinforced with ash ribs as well as the lower wires to prevent any twisting effect caused by rapid maneuvering either on the ground or in the air and it likewise acts as a protection in case of a "buckling" failure. The whole body is braced throughout by steel cables in the front section and wire in the rear.

The upper body ribs and on top of ash ribs cross member and are secured in the rear by C-clips. The whole unit is braced by three steel wire play made which bolt directly to the head and body struts in such a manner as to entirely eliminate all wire bracing.

Both control and main cable are made detachable for any purpose intended. The lower cable of the control cables are connected to a main rocker shaft, mounted in large bearings on the floor. Directly under the front and a center cable, the cables are connected with control cables consisting of the above control cables.

Just in back of the rear pit and mounted on the rear cable is a cross member which carries the control cables. The cables are connected to the rear control, by means of a universal joint, and two elevator cables which are connected to the control cables by a universal joint.

M.T.2 is equipped with the usual complement of instruments including compass for altitude work, and may also be equipped with the Lawson Detachable Hooting Arrangement, and compass of each end and two Pyramons connected to tubes running forward to the main section, which may also be



THREE-QUARTER REAR VIEW

located around the carburetor and gas tank as well as the fuel. In front of the front pit and on top of the fuselage a gas tank holding two hours' fuel is mounted. The nose of the body is covered with an aluminum covering which is slightly domed in form and is provided with air holes and inspection doors. The rear section is made in three sections. The first one is detached for inspection of the gas tank, while the second, which covers the pit, providing, can be replaced by a solid cover in case the rear end is used, thereby streamlining the section. Back of the wing a beam around the neck of spruce is attached by means of hinges, which allows easy inspection.

## Endorsements

This consists of the usual V-type having a 20° to 30° angle, which is mounted on a specially built-inward side and opening in rubber seal aluminum. The side as well as the upper tubes are secured by a universal joint.

The struts are of ash tapered into top sockets at both ends where they are bolted in large on the body and ash pins. Heavy cable bracing tubes of ash struts. This gear can be easily disconnected within 15 minutes using its simplicity.

On the rear of the body and on a tube secured in a standard ash tail and is usually secured. The ground is at such a design as to entirely eliminate any bending or breaking in case of a submergence. By removing these bolts the entire tripod and steel are removable in case of a replacement.

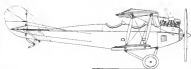
## Tail Group

This unit is constructed entirely of steel, the outer edges of all main being entirely of tubing either left round or flattened. The stabilizer is of the double cantilever type and is entirely of spruce framework with the exception of the ribs. Two spars joined by two ribs and wire take all lateral loads while the whole unit is carried below by streamlined tubes and also by cable running from the fuselage.

The stabilizer is set at a negative angle of two degrees and measures 20" x 16" 6".

The fin is entirely of tubing welded together. The surface is 16" high and the nose which is the stabilizer.

To both of these surfaces are hinged the elevators and rudder respectively. The former are built up of pressed steel ribs of channel section and lightened. These are 300 in. wide and give a total span in the tail of 15 ft. The rudder is 6 ft. high and 25 7/8 in. wide, semi-balanced and con-



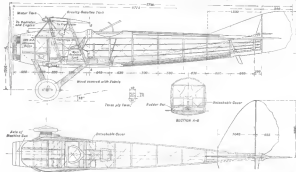
SIDE ELEVATION

## The Spad Two-Seater Fighter

The following particulars and illustrations, apparently from an official German report on the Spad two-seater, are published in Flugpost of April 30 and reproduced here from Flugpost.

The Spad two-seater, which is herewith described, is marked D 8006, and is built under license in July, 1917, by the Aus-

steuer together than those of the lower wing, and the inter plane struts converge somewhat upwards. The angle of incidence of the upper plane is 2.6 deg. at the root, and 2.5 deg. at the tip, while the lower plane has a uniform angle of 1.5 deg. The left wing is in dihedral, and is fitted to reduce hand resistance, the spine between them is fixed up-



SECTION A-B

craft Works of Ad. Hoesner in La Courneuve (Seine). In general design and in construction details it resembles the single-seater, but does not have the double main interplane struts usually found on these. It is built as an ordinary two-seater. The spans of the lower wings are based on the under-surface from the point of attachment of the main pair of struts. The upper wing, which runs right through, has a span of 31.25 m. and a chord of 2.53 m., while the lower wing has a span of 20.00 m. and a chord of 1.43 m. The gap is 1.30 m. and the stagger 0.4 m. There is no dihedral angle, but both upper and lower wings are swept back the angle being 17.4 deg. In order to give a better view, the lower wings have been cut away near the body, and the upper wing has a cut-out portion in the center. The two spars are placed

with strips of wood. The leading wires are single. A duct cable runs from the junction of the main interplane strut to the upper front spar, to the point of attachment of the front under-surface strut. The interplane struts, which are of aluminum alloy, are made of wood. Their struts are attached to a steel tube carried along the strut.

The spacing of the ribs is 180 mm. in the top wing and 170 mm. in the lower wing. Between the ribs there are fabric ribs on the upper surface running from leading edge to trailing edge. The fabric is tacked in some more strongly contoured ribs, and in its addition attached to ribs and to the main bracing the leading edge. On the under surface, near the trailing edge, there are struts which serve to equalize the pressure and to drain any moisture out of the wing. Wing

struts most of all and spars.

The machine is constructed at present as equipped with the 100-hp. engine, A.7A, model driving an 8 ft. propeller. However, being built for interchangeability, it can be equipped with a 200 hp. motor, and adapted for flying purposes.

and body covering are painted a yellowish white. The interplane struts are hinged to fabric spars in the upper plane. They are operated by means of push and pull rods which run to the lower plane behind the rear spar, and the movement of a block is transmitted through cranks at the lower end of the outer struts, in vertical struts pivoted to the lower surface of the struts.

The body, which is of the metal construction, with dimensions, 28 x 26 mm., and having at the rear to 24 x 24 mm., is rounded off top and bottom by fuselage and struts. The longitudinal is here a rectangular section, while



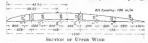
FRONT ELEVATION, SIDE ELEVATION, AND PLAN

the vertical and horizontal body struts are expanded out to a T section, and are reinforced by plywood. A trap-door in the floor behind the observer's cockpit provides access to the interior of the body.

The stabilizing and control surfaces are of the usual Spad type. The tail plane, which runs right across the body, and has both sides covered, is attached to the upper longitudinal at an angle of incidence of 9 deg. To the trailing edge, the double elevator is hinged by means of a steel tube. In order to reduce resistance, the cranks are placed in the center inside the body and vertical in

the machine is provided with dual control. For operating the ailerons, the movement of the control shaft is transmitted by means of a lever to a rocker supported in a partition between pilot's and observer's cockpits. The pole—which goes to the bottom wing—engages with a downward projection of the rocker. The observer's control lever is in the form of a telescopic tube, whose upper part is forced upwards by a spiral spring or ground down when not in use, and held in position by a bayonet joint. When extended, its length measured from the previous point 33 cm. and when retracted it measures 28 cm. The rudder bar in the observer's cockpit can be moved over with detachable covers, to guard

against accidental use. The V form under-surface struts are made up of several layers of wood, about 10 mm. thick, and are covered with fabric. Diagonal bracing is employed to hold front and rear legs. The two main struts rest between two cross tubes covered with fabric, and more in side in the struts. The front is 120 mm. The VEE type Hispano-Suiza engine, which develops about 200 hp. at 2,000 rpm., runs on engine mounts which are connected up to the body beam.



# Lawson

M. T. 1  
M. T. 2



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(Continued from page 697)

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(Continued from page 701)

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# INDEX TO ADVERTISERS

<b>A</b>			
Airbman Wheel Co.	499	L. W. P. Engineering Co.	5
Aqua Axle & Aero Metal Co.	498	Lawson Pumping & Tool Co.	6
Aluminum Castings Co.	493	Lawson Aircraft Co.	6
Aluminum Co. of America	496	Leeson Aircraft Corp.	6
American Propeller & Manufacturing Co.	797	Levert, Walker & Co.	6
Automobile Engineering Co.	797	Leymond & Co.	6
		Lewing, Brown & Co.	6
<b>B</b>			
Baker Control Oil Co.	491		
Barnes Mfg. Co.	497	Barton Glass Co.	6
Beta-Power Co., Inc.	491	Battison, C., Machine Works	6
Bloom, Johns, & Co.	793	Bass Radiator Division	6
Boston Aero Gage Co.	498	Bell Products Co.	6
Brook, Arthur, Jr.	795	Bellows Engineering Co.	6
Brooks Machine Co.	795	Bellows Storage Battery Co.	6
Burgess Co., Inc.	444		
		<b>N</b>	
<b>C</b>		National Wire Wheel Works	6
Chemical Products Co.	794	New Dispenser Mfg. Co.	6
Cold Light Manufacturing Co.	793	Norris Co. of America	6
Continental Aircraft Corp.	449		
Carlson Aeroplane & Motor Corp.	712	Orbison Engineering Co.	6
<b>D</b>			
Dallas Manufacturing Corp.	793	Palmer Sausage Co.	6
Dayton Hotel Powder Co.	643	Park Iron Works	6
Defiance Machine Works	793	Penn. Aircraft Supply Co.	6
Decker Die Casting Co.	793	Perkins P. Machine Co.	6
Derby, W. A.	795		
Desenberg Motors Corp.	646	Quinn Insurance Co.	6
Desai Rubber Corp.	793		
		<b>R</b>	
<b>E</b>		Radium Dial Co.	6
East Aviation School	799	Radium Lampworks National Corp.	6
Excelsior Manufacturing Co.	799	Reidman's John A. Ross Co.	6
Erie Specialty Co.	673	Rear Taper Reducer Co.	6
		Ross H. Manufacturing Co.	6
<b>F</b>			
Fairair Bearing Co.	681	S. K. P. Ball Bearing Co.	6
Fairing Metal Co.	654	Schroeder & Co.	6
Federal Mfg. Co.	656	So. Louisiana Mfg. & Eng. Co.	6
Federal, L. W. & Co.	793	Sperry Gyroscope Co.	6
Fleming Manufacturing Co.	656	Springer Wire Wheel Corp.	6
Fordham, The Co.	793	Standard Aircraft Corp.	6
Fox Machine Co.	793	Standard Turbine Co.	6
		Stangor, Edgar B. Co.	6
		Stevens & Bangs	6
<b>G</b>			
General Radios Co.	699		
Gillette Safety Razor Co.	695		
Grand Rapids Vener Works	692		
G. and O. Mfg. Co.	693		
		<b>T</b>	
<b>H</b>		Taylor Instrument Company	6
Hall-Scott Motor Car Co.	643	Thomas-Morse Aircraft Corp.	6
Hammacher, Schlemmer & Co.	692	Trapp Steel & Iron Co.	6
Hardy, F. A. & Co.	794		
Hart-Walton Propeller Co.	793		
Hendler Manufacturing Co.	792		
Hess-Bright Mfg. Co.	711		
		<b>U</b>	
<b>I</b>		Union Gas Engine Co.	6
International Acoustical Instrument Corp.	704		
		<b>W</b>	
<b>J</b>		Wet Woodworking Co.	6
Jameson Propeller Co.	692	White, J. G., The Engineering Corp.	6
Jameson Bros.	693	Whitman & Barnes Manufacturing Co.	6
		Whitman, J. C. & Co.	6
		Whitman Motor Manufacturing Co.	6
		Whitman-Towne Aircraft Co.	6
		Wood, J. W., Elastic Web Co.	6
		Wright-Martin Aircraft Corp.	6
		Wyman Gordon Co.	6
<b>K</b>			
Kawner Mfg. Co.	651	Zenith Carburetor Co.	6



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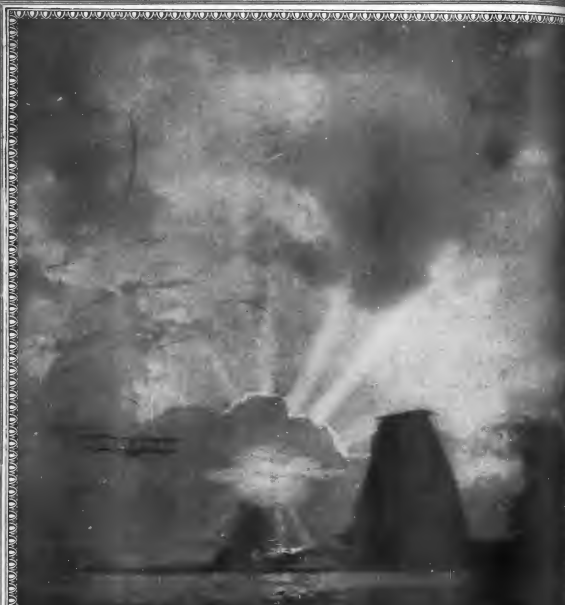
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